

# N Atom Measurements in High-Temperature N<sub>2</sub> Dissociation Kinetics

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The dissociation of N<sub>2</sub> has been measured behind reflected shock waves in a temperature range of  $3390 \leq T \leq 6435$  K. By use of the atomic resonance absorption spectroscopy (ARAS), the formation of N atoms could directly be observed in the postshock reaction zone. The experiments have been performed in mixtures of N<sub>2</sub> and Ar at pressures between 0.9 and 2.1 bar. The rate coefficient of the reaction,  $N_2 + Ar \rightarrow N + N + Ar$  [ $k_{N_2,Ar} = 1.71 \cdot 10^4 T^{-3.33} \exp(-113,220 K/T) \text{ cm}^3/\text{s} \pm 20\%$ ] could directly be determined from the measured N atom concentrations.

## Introduction

THE N<sub>2</sub> molecule is known to be very stable up to very high temperatures. Nevertheless, the dissociation of N<sub>2</sub> can be of considerable interest in plasma reaction kinetics or in hypersonic wind tunnels. Because of the very high activation energy of the N<sub>2</sub> dissociation, experimental data are available only at temperatures higher than 6000 K.

Essentially, there are four experimental results of the N<sub>2</sub> dissociation that were evaluated by Baulch et al.<sup>1</sup> These investigations were performed in shock tubes using different detection techniques. Cary<sup>2</sup> and Byron<sup>3</sup> observed the reaction in N<sub>2</sub>/Ar mixtures, recording the density profiles by interferometry. Hanson and Boganoff<sup>4</sup> measured pressure profiles in the reaction zone of pure N<sub>2</sub>. A spectroscopic method was used by Appleton et al.<sup>5</sup> in mixtures of N<sub>2</sub> and Ar. They monitored the rate of N<sub>2</sub> dissociation more directly by the vacuum ultraviolet absorption of N<sub>2</sub> at 117.6 nm. Their expression of the rate coefficient was recommended by Baulch et al.<sup>1</sup> for use in the 6000-15,000 K temperature range. The proposed rate coefficients of Byron,<sup>3</sup> Cary,<sup>2</sup> and Hanson and Boganoff<sup>4</sup> were found to be higher than the recommended value of Baulch et al.<sup>1</sup>

It is the aim of the present study to determine the rate coefficient of the N<sub>2</sub> dissociation in N<sub>2</sub>/Ar mixtures by measuring the N atoms as reaction products, mainly in the temperature region below the 6000 K limit.

## Experimental

The experiments were conducted behind reflected shock waves in a stainless steel shock tube of 79 mm i.d. The tube is constructed as an ultrahigh vacuum apparatus and can be heated and evacuated down to pressures of about  $10^{-8}$  mbar. Typical rates of leaks plus outgassing were  $8 \cdot 10^{-7}$  mbar/min. A detailed description of the equipment is given in Ref. 6. The test gases used in the experiments were supplied by Messer Griesheim, FRG. They were certificated to be of the purities  $N_2 \geq 99.9995\%$  and  $Ar \geq 99.9999\%$ .

The atomic resonance absorption spectroscopy (ARAS) is the measurement technique applied in this investigation of the NI triplet at 119.9 nm. It is a very sensitive line-emission-line absorption method for measuring N atom concentrations in the range of  $5 \cdot 10^{11}$ - $3 \cdot 10^{13}$  atoms/cm<sup>3</sup>. The spectral

shape of the emitter line is not known in detail. It is supposed to be influenced by self-reversal. Hence, calibration measurements were necessary to obtain the required relation between the measured resonance absorption and the corresponding N atom concentrations. The calibration measurements were conducted in a temperature range of  $4300 \leq T \leq 8200$  K and at pressures similar to those used in the present experiments. Although there was some scattering in the calibration data, a temperature or pressure dependence of the calibration curve could not be observed. The optical arrangement, the operating conditions of the resonance lamp, and the calibration procedure were described previously.<sup>7</sup>

The mean temperature behind the reflected shock wave was computed from the incident shock speed using one-dimensional gasdynamic equations. The optical windows were located 15 mm from the end plate of the shock tube. Under these conditions, cooling of the reaction volume by heat transfer in the temperature boundary layer can assumed to be small.

It is known that shock/boundary-layer effects can cause changes in the steadiness conditions behind the reflected shock. This was ignored in the data evaluation. The rate coefficient was determined from the N atom increase measured at short dissociation times. Therefore, any changes in the postshock conditions are assumed to have negligible effect on the results reported here.

## Results

The dissociation of N<sub>2</sub> was studied in the temperature range  $3390 \leq T \leq 6435$  K at pressures of 0.9-2.1 bar. In 34 shock tube experiments, the relative initial concentrations of N<sub>2</sub> were between 87 ppm and 100%. In each experiment, the measured incident shock speed served to calculate the temperature and pressure behind the reflected shock. The N atom resonance absorption signals were monitored from the reacting gas mixture. A representative absorption profile is shown in Fig. 1. Using the calibration curve given in Ref. 7, each absorption signal can be easily transformed to a N atom concentration profile. One example is shown in Fig. 2. In all cases, the N atom increase is nearly linear during the total experimental time. Only in some experiments, mainly at temperatures below 4000 K, an induction period of about 40-100  $\mu\text{s}$  was observed after the arrival of the shock. This must be caused by the vibrational relaxation or reaction incubation processes. Acceptable agreement with predicted values based on the measurements of Millikan and White<sup>8</sup> and Appleton<sup>9</sup> was found.

A first rough reduction of the measured N atom concentration data was made by dividing the slope of the N atom

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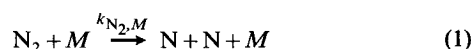
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increase  $d[N]/dt$  by the product  $2[N_2][M]$ . As the maximum measurable value is about  $3.10^{13}$  N atoms/cm<sup>3</sup>, the N atom concentrations in the experiments were very low with respect to the initial concentrations of N<sub>2</sub>. Therefore, the N<sub>2</sub> concentration can always be assumed to be nearly constant over the experimental period of time. Consequently,  $[M] = [Ar] + [N_2]$  is the quasitotal concentration of the reacting mixture. In Table 1, the experimental conditions and the reduced data of the experiments are summarized.

### Discussion

The first step in data interpretation is made by considering a reaction with unspecified collision partner,



and evaluating the quantity

$$k_{N_2,M} = \frac{d[N]/dt}{2[N_2][M]} \quad (2)$$

as a function of the reciprocal temperature. Equation (2)

represents the rate coefficient of the N<sub>2</sub> dissociation if Ar and N<sub>2</sub> are assumed to have the same collision efficiency. The results are given in Table 1. If the values of  $k_{N_2,M}$  were plotted in a Arrhenius diagram, a slight non-Arrhenius behavior could be found. For experiments with relative concentrations of N<sub>2</sub> ≤ 5%, the data points scatter around a straight line, whereas for N<sub>2</sub> > 5% (i.e., at the low temperature end of the Arrhenius plot), the experimental points appear to be systematically deviated from the straight line. This behavior can be explained by the more effective collision partner N<sub>2</sub>.

A more detailed kinetic interpretation of the dissociation experiments was done by considering the reactions



The rate coefficient of Eq. (3) can therefore be described as

$$k_{N_2,Ar} = \frac{d[N]/dt}{2[N_2]([Ar] + \eta[N_2])} \quad (5)$$

Table 1 Experimental conditions and rate coefficients

<i>T</i> , K	<i>p</i> , bar	N <sub>2</sub> , %	N <sub>2</sub> , cm <sup>-3</sup>	Ar, cm <sup>-3</sup>	$\frac{d[N]/dt}{2[N_2][M]}$ , cm <sup>3</sup> ·s <sup>-1</sup>	<i>k</i> <sub>N<sub>2</sub>,Ar</sub> , cm <sup>3</sup> ·s <sup>-1</sup>
3392	1.51	100	$3.24 \times 10^{18}$	—	$2.45 \times 10^{-22}$	—
3478	2.10		$4.38 \times 10^{18}$	—	$5.99 \times 10^{-22}$	—
3548	1.37		$2.76 \times 10^{18}$	—	$1.10 \times 10^{-21}$	—
3530	1.97	75	$3.03 \times 10^{18}$	$1.01 \times 10^{18}$	$7.35 \times 10^{-22}$	$3.46 \times 10^{-22}$
3421	2.26	50	$2.39 \times 10^{18}$	$2.39 \times 10^{18}$	$3.00 \times 10^{-22}$	$1.71 \times 10^{-22}$
3673	1.07		$1.05 \times 10^{18}$	$1.05 \times 10^{18}$	$1.42 \times 10^{-21}$	$8.11 \times 10^{-22}$
3675	2.12		$2.09 \times 10^{18}$	$2.09 \times 10^{18}$	$1.66 \times 10^{-21}$	$9.48 \times 10^{-22}$
3861	1.72		$1.60 \times 10^{18}$	$1.60 \times 10^{18}$	$5.30 \times 10^{-21}$	$3.03 \times 10^{-21}$
3953	1.99		$1.81 \times 10^{18}$	$1.81 \times 10^{18}$	$7.60 \times 10^{-21}$	$4.34 \times 10^{-21}$
3730	1.24	25	$6.03 \times 10^{17}$	$1.81 \times 10^{18}$	$2.85 \times 10^{-21}$	$2.07 \times 10^{-21}$
3805	1.13		$5.38 \times 10^{17}$	$1.61 \times 10^{18}$	$4.40 \times 10^{-21}$	$3.21 \times 10^{-21}$
4073	1.08		$4.80 \times 10^{17}$	$1.44 \times 10^{18}$	$1.63 \times 10^{-20}$	$1.18 \times 10^{-20}$
4142	1.07	5	$9.37 \times 10^{16}$	$1.78 \times 10^{18}$	$1.67 \times 10^{-20}$	$1.48 \times 10^{-20}$
4178	1.23		$1.07 \times 10^{17}$	$2.02 \times 10^{18}$	$2.20 \times 10^{-20}$	$1.93 \times 10^{-20}$
4240	1.20	2	$4.12 \times 10^{16}$	$2.02 \times 10^{18}$	$5.26 \times 10^{-20}$	$5.00 \times 10^{-20}$
4384	1.38		$4.56 \times 10^{16}$	$2.23 \times 10^{18}$	$8.11 \times 10^{-20}$	$7.72 \times 10^{-20}$
4510	1.17		$3.75 \times 10^{16}$	$1.84 \times 10^{18}$	$1.48 \times 10^{-19}$	$1.41 \times 10^{-19}$
4171	1.03	1	$1.78 \times 10^{16}$	$1.76 \times 10^{18}$	$2.99 \times 10^{-20}$	$2.93 \times 10^{-20}$
4238	1.17		$1.99 \times 10^{16}$	$1.97 \times 10^{18}$	$4.34 \times 10^{-20}$	$4.23 \times 10^{-20}$
4346	1.23		$2.05 \times 10^{16}$	$2.03 \times 10^{18}$	$7.57 \times 10^{-20}$	$7.38 \times 10^{-20}$
4526	1.16		$1.85 \times 10^{16}$	$1.83 \times 10^{18}$	$2.04 \times 10^{-19}$	$1.99 \times 10^{-19}$
4703	1.08		$1.66 \times 10^{16}$	$1.64 \times 10^{18}$	$3.60 \times 10^{-19}$	$3.51 \times 10^{-19}$
4894	1.04		$1.54 \times 10^{16}$	$1.53 \times 10^{18}$	$6.37 \times 10^{-19}$	$6.21 \times 10^{-19}$
4557	1.03	0.5	$8.18 \times 10^{15}$	$1.63 \times 10^{18}$	$1.99 \times 10^{-19}$	$1.96 \times 10^{-19}$
4806	0.95		$7.17 \times 10^{15}$	$1.43 \times 10^{18}$	$6.10 \times 10^{-19}$	$6.02 \times 10^{-19}$
5412	0.93		$6.23 \times 10^{15}$	$1.24 \times 10^{18}$	$6.05 \times 10^{-18}$	$5.96 \times 10^{-18}$
5243	1.06	0.25	$3.65 \times 10^{15}$	$1.46 \times 10^{18}$	$2.33 \times 10^{-18}$	$2.31 \times 10^{-18}$
5496	0.95		$3.13 \times 10^{15}$	$1.25 \times 10^{18}$	$6.82 \times 10^{-18}$	$6.77 \times 10^{-18}$
5385	0.91	0.20	$2.44 \times 10^{15}$	$1.22 \times 10^{18}$	$4.33 \times 10^{-18}$	$4.31 \times 10^{-18}$
5600	1.87	0.01	$2.42 \times 10^{14}$	$2.42 \times 10^{18}$	$1.31 \times 10^{-17}$	$1.31 \times 10^{-17}$
5835	1.91		$2.37 \times 10^{14}$	$2.37 \times 10^{18}$	$2.05 \times 10^{-17}$	$2.05 \times 10^{-17}$
6063	1.77		$2.12 \times 10^{14}$	$2.12 \times 10^{18}$	$3.67 \times 10^{-17}$	$3.67 \times 10^{-17}$
6434	1.70		$1.92 \times 10^{14}$	$1.92 \times 10^{18}$	$9.04 \times 10^{-17}$	$9.04 \times 10^{-17}$
5843	1.69	0.0087	$1.83 \times 10^{14}$	$2.10 \times 10^{18}$	$1.87 \times 10^{-17}$	$1.87 \times 10^{-17}$

where  $\eta$  is the dissociation efficiency of  $N_2$  relative to Ar,

$$\eta = k_{N_2, N_2} / k_{N_2, Ar} \quad (6)$$

Normally, the efficiency  $\eta$  can be assumed to be independent of temperature. With the assumption of  $\eta = 2.5$ , the rate coefficient  $k_{N_2, Ar}$  was determined as given in the last column of Table 1.

It has been common practice to express dissociation rates in the form

$$k = A \cdot T^n \cdot \exp(-D/T) \quad (7)$$

with  $D$  as the dissociation temperature. A least squares fit of the  $k_{N_2, Ar}$  data, presented in Table 1, leads to the expression

$$k_{N_2, Ar} = 1.71 \cdot 10^4 T^{-3.33} \exp(-113,200 K/T) \text{ cm}^3/\text{s} \pm 20\% \quad (8)$$

where  $3390 \leq T \leq 6435$  K.

The given uncertainty is the percentage standard deviation. The absolute value of the temperature exponent seems to be too high from the theoretical point of view. It results from the used approximation method used to fit the data points.

A comparison between Eq. (8) and the rate coefficients obtained by several other investigators<sup>2,3,5</sup> is shown in Fig. 3. It is obvious that an extrapolation of our expression up to more elevated temperatures crosses the rate coefficient proposed by Appleton et al.<sup>5</sup>

For the temperature range of this experimental study, the presented value of  $k_{N_2, Ar}$  [Eq. (8)] is in good agreement with estimates obtained from Troe's weak collision unimolecular reaction rate theory,<sup>10</sup> although it is known that this theory is normally valid only for molecules with more than one vibrational degree of freedom. According to this theory, the dissociation rate coefficient for the low-pressure region can be expressed as

$$k_{N_2, Ar} = k_{N_2, Ar}^{sc} \cdot \beta_c \quad (9)$$

Table 2 Measured and calculated rate coefficients for unimolecular low-pressure dissociation of  $N_2$

$T$ , K	$k_{N_2, Ar}$ , $\text{cm}^3/\text{s}$	$k_{N_2, Ar}^{sc}$ , $\text{cm}^3/\text{s}$	$\beta_c$
3330	$5.49 \times 10^{-23}$	$9.32 \times 10^{-22}$	$5.89 \times 10^{-2}$
4000	$8.86 \times 10^{-21}$	$2.75 \times 10^{-19}$	$3.22 \times 10^{-2}$
5000	$1.21 \times 10^{-18}$	$7.60 \times 10^{-17}$	$1.59 \times 10^{-2}$
7000	$2.54 \times 10^{-16}$	$4.51 \times 10^{-14}$	$5.64 \times 10^{-3}$

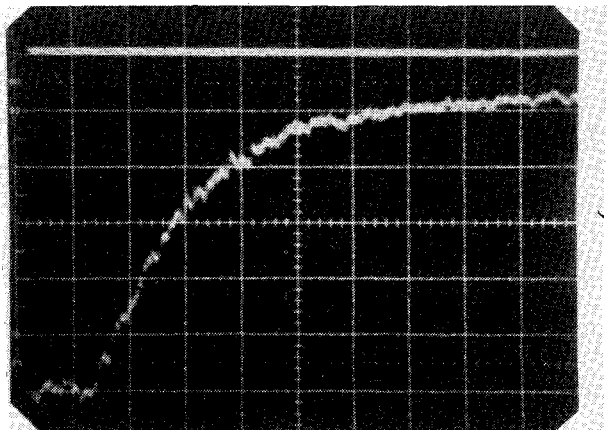


Fig. 1 Measured N atom absorption signal:  $[N_2]_0 = 1.54 \times 10^{16} \text{ cm}^{-3}$ ,  $[Ar] = 1.53 \times 10^{18} \text{ cm}^{-3}$ ,  $T = 4894$  K,  $p = 1.04$  bar,  $100 \mu\text{s}/\text{div}$ .

where  $k_{N_2, Ar}^{sc}$  denotes the strong collision rate coefficient and  $\beta_c$  the weak collision factor. The strong collision rate coefficient depends on several molecular quantities and can be calculated according to Ref. 10. The weak collision factor includes all of the uncertainties in the theory and experiments and will, in general, be fitted to the experimentally determined reaction coefficient. In the present case, the strong collision rate coefficient  $k_{N_2, Ar}^{sc}$  was computed based on the equations given by Troe.<sup>10</sup> The weak collision factor  $\beta_c$  can be determined using Eq. (9). Results are given in Table 2. The values of  $\beta_c$  show the expected temperature behavior and the absolute quantity seems to be in agreement with the unimolecular reaction theory of Troe.<sup>10</sup>

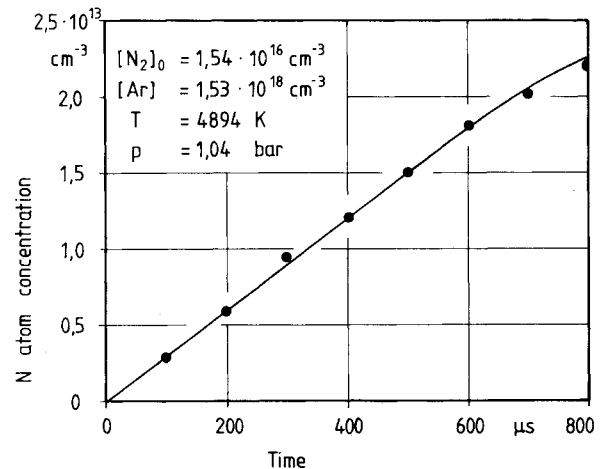


Fig. 2 Example of a measured N atom concentration profile in a shock heated  $N_2/Ar$  mixture.

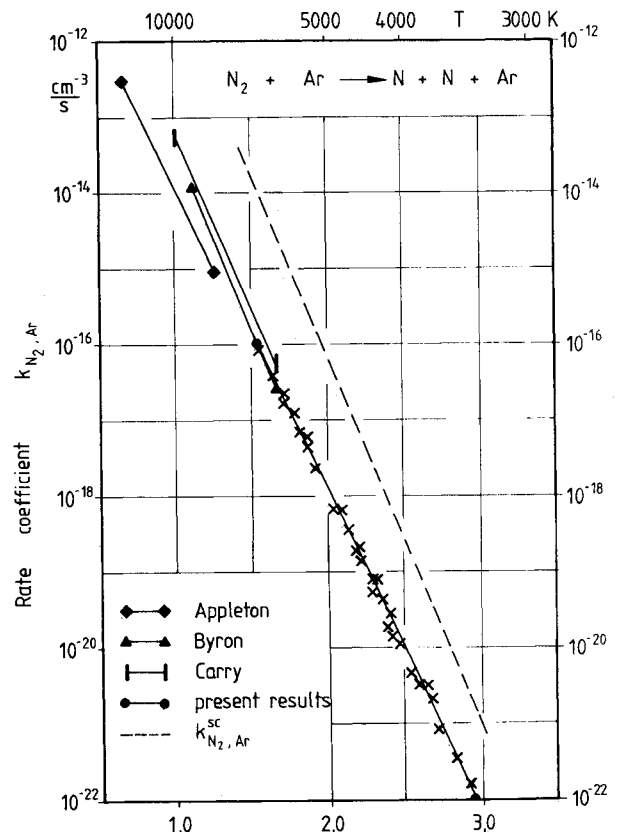


Fig. 3 Comparison of rate coefficients for  $N_2 + Ar \rightarrow N + N + Ar$ .

### Conclusion

Resonance absorption measurements of N atoms was shown to be a sensitive method to study N<sub>2</sub> dissociation kinetics in the temperature range  $3390 \leq T \leq 6435$  K behind reflected shock waves. It seems to be the first time in N<sub>2</sub> dissociation that the reaction product could be directly observed. The rate coefficient for N<sub>2</sub> dissociation with Ar as a collision partner was determined with acceptable uncertainties when the collision efficiency of the species N<sub>2</sub> relative to Ar is assumed to be  $\eta = 2.5$ . Comparison of the experimental data with the theoretical data obtained using the weak collision unimolecular rate theory of Troe<sup>10</sup> leads to reasonable weak collision factors  $\beta_c$ .

### Acknowledgment

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## TRANSONIC AERODYNAMICS—v. 81

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Forty years ago in the early 1940s the advent of high-performance military aircraft that could reach transonic speeds in a dive led to a concentration of research effort, experimental and theoretical, in transonic flow. For a variety of reasons, fundamental progress was slow until the availability of large computers in the late 1960s initiated the present resurgence of interest in the topic. Since that time, prediction methods have developed rapidly and, together with the impetus given by the fuel shortage and the high cost of fuel to the evolution of energy-efficient aircraft, have led to major advances in the understanding of the physical nature of transonic flow. In spite of this growth in knowledge, no book has appeared that treats the advances of the past decade, even in the limited field of steady-state flows. A major feature of the present book is the balance in presentation between theory and numerical analyses on the one hand and the case studies of application to practical aerodynamic design problems in the aviation industry on the other.

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